

# Extraction of Hydrocarbons from High-Maturity Marcellus Shale Using Supercritical Carbon Dioxide

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**ABSTRACT:** Shale is now commonly exploited as a hydrocarbon resource. Due to the high degree of geochemical and petrophysical heterogeneity both between shale reservoirs and within a single reservoir, there is a growing need to find more efficient methods of extracting petroleum compounds (crude oil, natural gas, bitumen) from potential source rocks. In this study, supercritical carbon dioxide (CO<sub>2</sub>) was used to extract *n*-aliphatic hydrocarbons from ground samples of Marcellus shale. Samples were collected from vertically drilled wells in central and western Pennsylvania, USA, with total organic carbon (TOC) content ranging from 1.5 to 6.2 wt %. Extraction temperature and pressure conditions (80 °C and 21.7 MPa, respectively) were chosen to represent approximate *in situ* reservoir conditions at sample depth (1920–2280 m). Hydrocarbon yield was evaluated as a function of sample matrix particle size (sieve size) over the following size ranges: 1000–500 μm, 250–125 μm, and 63–25 μm. Several methods of shale characterization including Rock-Eval II pyrolysis, organic petrography, Brunauer–Emmett–Teller surface area, and X-ray diffraction analyses were also performed to better understand potential controls on extraction yields. Despite high sample thermal maturity, results show that supercritical CO<sub>2</sub> can liberate diesel-range (*n*-C<sub>11</sub> through *n*-C<sub>21</sub>) *n*-aliphatic hydrocarbons. The total quantity of extracted, resolvable *n*-aliphatic hydrocarbons ranges from approximately 0.3 to 12 mg of hydrocarbon per gram of TOC. Sieve size does have an effect on extraction yield, with highest recovery from the 250–125 μm size fraction. However, the significance of this effect is limited, likely due to the low size ranges of the extracted shale particles. Additional trends in hydrocarbon yield are observed among all samples, regardless of sieve size: 1) yield increases as a function of specific surface area ( $r^2 = 0.78$ ); and 2) both yield and surface area increase with increasing TOC content ( $r^2 = 0.97$  and 0.86, respectively). Given that supercritical CO<sub>2</sub> is able to mobilize residual organic matter present in overmature shales, this study contributes to a better understanding of the extent and potential factors affecting the extraction process.

## ■ INTRODUCTION

Hydraulic fracturing has proven to be a successful well stimulation technique, enhancing matrix permeability of unconventional reservoirs and thus, improving production of oil and natural gas.<sup>1,2</sup> However, due to variability in both organic and inorganic components found among different shale formations and within a single reservoir, there remains a need to develop different fracturing fluid systems that can optimize well productivity.<sup>2</sup> In this regard, carbon dioxide (CO<sub>2</sub>) may provide an extraction alternative to conventional water-based fluids in both water-sensitive (i.e., those with an abundance of expanding clay minerals) and oil-wet formations that preferentially imbibe oil.<sup>2–4</sup> Consequently, the potential use of CO<sub>2</sub> as a non-aqueous working fluid in hydraulic fracturing and unconventional oil and gas (UOG) development is currently being investigated.<sup>2,4–11</sup>

Supercritical fluid extractions use high-density gases to extract a variety of organic compounds from solid matrices. Higher, liquid-like solvent densities observed in the supercritical region enhance solvent strength or dissolving power, enabling the supercritical fluid to vaporize some higher molecular weight, low volatility compounds at temperatures below their normal boiling points.<sup>12,13</sup> However, by virtue of the gaseous properties of the solvent, supercritical fluids maintain higher diffusivity, lower viscosity, and lower surface tension compared to conventional liquid solvents, improving

mass transfer through the sample matrix and increasing extraction rates.<sup>13–16</sup> Carbon dioxide exists in a supercritical state at temperatures and pressures greater than its critical point of 30.978 ± 0.015 °C (critical temperature,  $T_c$ ) and 7.3773 ± 0.0030 MPa (critical pressure,  $P_c$ ).<sup>17</sup> At this critical point, CO<sub>2</sub> has a critical density of 467.6 ± 0.6 kg/m<sup>3</sup>.<sup>17</sup>

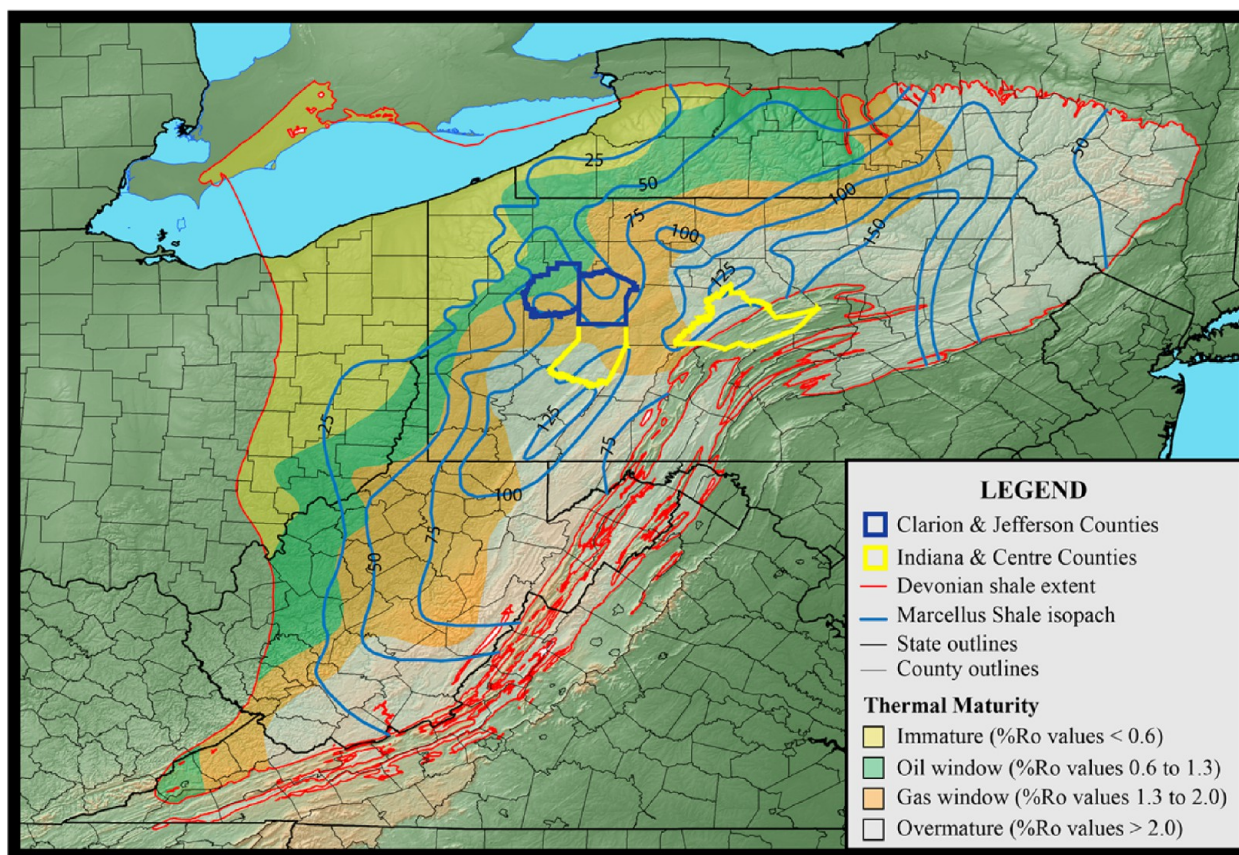
Supercritical CO<sub>2</sub> has successfully extracted and separated a wide range of non-polar aliphatic and polycyclic aromatic hydrocarbons from shale and coal under varying extraction parameters.<sup>13–15,18–21</sup> The effective molecular diameter of CO<sub>2</sub>, 3.3 Å,<sup>22</sup> enables CO<sub>2</sub> to access micropores of coal and shale matrices.<sup>22–26</sup> Monin et al.<sup>14</sup> extracted *n*-aliphatic hydrocarbons from diverse shale source rocks (of the Mahakam Delta, Indonesia, the Douala Basin, Cameroon, and the Paris Basin, France) in the range of *n*-C<sub>10</sub> through *n*-C<sub>34</sub> with supercritical CO<sub>2</sub> (at 40 °C and 20 MPa). Li et al.<sup>15</sup> extracted similar ranges of aliphatic and aromatic hydrocarbons from U.S. shales and coals of the Fruitland and Pottsville Formations (Cretaceous and Pennsylvanian periods, respectively) at 120 °C and 20.3 MPa, but focused on quantifying the recovery of more volatile (C<sub>6</sub> to C<sub>14</sub>) hydrocarbons, with yields ranging between 0.01 and 0.2 wt % (grams of extracted hydrocarbon per gram of

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**Figure 1.** Map of the Marcellus Shale, with thermal maturity zones, isopach lines,<sup>43</sup> and sampled Pennsylvania counties. Map modified from East et al.<sup>44</sup> Samples from the 3S (Clarion County), 2LT and 4LG (Jefferson County), and 2LK (Centre County) cores were donated courtesy of EXCO Resources, Inc. Samples from the EG (Indiana County) core were donated courtesy of the Pennsylvania Geological Survey, Department of Conservation and Natural Resources.

sample). However, both studies normalized their yields to the sample mass, with no report of organic richness, type, thermal maturity, or mineralogy. Consideration of organic and inorganic shale matrices is important in assessing extraction potential as these compositional elements directly impact pore structure and connectivity, hydrocarbon sorption capacities, and transport processes within shale reservoirs.<sup>27–30</sup>

Normalizing oil content or extractable organic matter (EOM) to total organic carbon (TOC) content thus provides a more accurate indication of production potential relative to absolute yields.<sup>31</sup> Furthermore, sorption capacities of both oil and gas are also known to increase with TOC, as does micro- and nanoscale porosity (volume and surface area) within organic matter, in thermally mature shales.<sup>27–29,31</sup> Results of this study have thus been normalized to TOC to better evaluate extracted hydrocarbon yield relative to the organic matter present within the shale samples. Given the heterogeneous geochemical and geophysical characteristics of shale reservoirs, this will hopefully also provide a better means of comparing extraction yields from shales across different maturity levels in future extraction studies.

Supercritical CO<sub>2</sub> extraction studies have assessed the effect of sample particle size distribution (from approximately 0.07 mm to 2.0 mm in diameter) on extraction efficiency from various solid matrices (oil shale, paprika, cocoa nibs).<sup>32–34</sup> All show an increase in recovery of organic compounds with decrease in sieve size. Authors of these studies attribute this trend to an increase in exposed sample surface area associated

with smaller particles, which enhances accessibility of the solvent to the extractable compounds, creates shorter diffusion paths, enhances mass transfer through the sample matrix, and thus ultimately increases overall extraction rates. However, other authors<sup>35,36</sup> have suggested that there may be an optimum particle size (sieve size) in supercritical fluid extractions, ranging from approximately 2.0 mm to 250 μm. If particle sizes are too small, channeling of solvent flow can occur within the extraction cell. These directed flow paths can reduce interactions between the solvent and extractable compounds, resulting in a decline in extraction efficiency and overall recovery.<sup>35,36</sup> Lower extraction efficiencies sometimes encountered with sieve sizes below this range have also been associated with particle aggregation,<sup>37</sup> and with higher capillary entry pressures, which can require greater force to extract hydrocarbons from porous media.<sup>38</sup> The process of grinding samples into smaller particles may change grain size distributions based on mineral hardness, and also lead to loss of volatile compounds,<sup>35</sup> both of which may affect extraction yields.

Consequently, a deeper investigation into the effect of shale matrix particle size on hydrocarbon recovery in supercritical fluid extractions is needed to better understand the mechanisms of CO<sub>2</sub>–hydrocarbon interactions within shale matrices. This study seeks to contribute to a better understanding of the extent and controls on the mobilization process, which is important if CO<sub>2</sub> is to be used as a working fluid for hydraulic fracturing and UOG development.<sup>2,5–11</sup> Understanding these



Table 1. Rock-Eval II Pyrolysis Results for Selected Core Samples for Supercritical CO<sub>2</sub> Extractions

core-sample ID <sup>a</sup>	county, PA	vertical depth (m)	resource potential				type of organic matter			thermal maturation	
			TOC <sup>b</sup>	S1 <sup>c</sup>	S2 <sup>c</sup>	S1/TOC <sup>d</sup>	S3 <sup>e</sup>	HI <sup>f</sup>	OI <sup>g</sup>	PI	T <sub>max</sub> <sup>h</sup>
3S-8	Clarion	1924	4.8	2.8	0.7	58.8	0.4	14.6	7.9	0.8	517
3S-29	Clarion	1951	6.2	0.7	0.7	11.8	0.3	11.5	5.2	0.5	547
2LT-12	Jefferson	2267	3.2	0.8	0.5	24.3	0.2	16.4	6.3	0.6	364
2LT-19	Jefferson	2277	3.7	0.7	0.6	19.0	0.3	16.0	8.4	0.5	380
4LG-3	Jefferson	2008	3.9	0.9	0.4	23.8	0.3	9.6	7.5	0.7	359
4LG-18	Jefferson	2025	1.5	1.0	0.3	64.5	0.6	17.1	38.2	0.8	341
4LG-25	Jefferson	2031	5.6	1.2	0.4	20.9	0.2	7.5	3.0	0.7	533

<sup>a</sup>Samples courtesy of EXCO Resources, Inc. <sup>b</sup>TOC (wt %). <sup>c</sup>S1 and S2 (mg HC/g rock). <sup>d</sup>S1/TOC (mg HC/g TOC). <sup>e</sup>S3 (mg CO<sub>2</sub>/g rock). <sup>f</sup>HI (mg HC/g TOC). <sup>g</sup>OI (mg CO<sub>2</sub>/g TOC). <sup>h</sup>T<sub>max</sub> (°C).

interactions is also important in terms of caprock integrity at geologic CO<sub>2</sub> storage sites. Injection of CO<sub>2</sub> has the potential to react with the caprock, potentially altering matrix porosity and permeability, and increasing levels of dissolved organic carbon and alkalinity within *in situ* brines.<sup>39–42</sup>

The primary objective of this study is to determine the quantity and distribution of *n*-aliphatic hydrocarbons that can be extracted from Marcellus Shale samples with supercritical CO<sub>2</sub> as a function of sample matrix particle size (sieve size), at estimated *in situ* pressure and temperature conditions. Selected particle size ranges (1000–500 μm, 250–125 μm, and 63–25 μm) include two ranges below the optimum range suggested above.<sup>35,36</sup> Results are evaluated as a function of the following: (1) Rock-Eval II pyrolysis and TOC analysis to evaluate source rock potential (quantity, quality and thermal maturity of organic matter); (2) reflectance analysis to determine thermal maturity and identify organic matter type; (3) X-ray diffraction (XRD) to determine mineral abundances; (4) Brunauer–Emmett–Teller (BET) surface area analysis of the selected sieve sizes; and (5) scanning electron microscopy (SEM) imaging to visualize shale surface and porosity characteristics.

## EXPERIMENTAL SECTION

**Sampling.** Cores intersecting the Marcellus Shale were donated from EXCO Resources, Inc., and the Pennsylvania Geological Survey, Department of Conservation and Natural Resources. All samples are from vertically drilled wells located in central and western Pennsylvania, with subsurface depths ranging from approximately 1920 m to 2280 m (Figure 1). Exact well locations and drilling fluid compositions are unknown. Specimens from different sedimentary facies throughout the five cores were sampled for potential use in the supercritical CO<sub>2</sub> extraction experiments.

**Rock-Eval II Pyrolysis and Total Organic Carbon Analysis.** Samples were sent to GeoMark Research, Ltd. for Rock-Eval II pyrolysis and TOC analysis to provide an initial screening of shale source rock potential. Pyrolysis was performed on a Rock-Eval II instrument, and TOC analysis on a LECO C230 instrument. Rock-Eval II measured parameters include (1) the S1 peak, representing free, thermally extractable hydrocarbons present in the rock, expressed in units of milligrams of hydrocarbon (HC) per gram of rock; (2) the S2 peak, representing the abundance of hydrocarbons generated from pyrolytic cracking of the remaining kerogen, expressed in units of milligrams of HC per gram of rock; (3) T<sub>max</sub> (°C), which is the temperature recorded at the maximum generation of hydrocarbons within the S2 peak; and (4) the S3 peak, representing CO<sub>2</sub> content, expressed in units of milligrams of organic CO<sub>2</sub> per gram of rock.<sup>45,46</sup> Based on results, seven samples (from the 3S, 2LT, and 4LG cores) were selected for further geochemical characterization and subsequent supercritical CO<sub>2</sub> extractions (Table 1). Chosen samples were considered to have the greatest extraction potential, with selection criteria based on the highest S1 (>0.70 mg HC/g rock) and S1/TOC

(mg HC/g TOC) values. The S1/TOC value, also referred to as the oil saturation index, normalizes oil content to TOC and is used as an indicator of *in situ* source rock potential.<sup>31</sup>

**Sample Preparation.** Each sample was crushed to a powder with a stainless steel mortar and pestle. Crushed samples were subsequently dry-sieved by using a nested stack of U.S.A. Standard sieves into the following size fractions: 1000–500 μm (18–35 mesh), 250–125 μm (60–120 mesh), and 63–25 μm (230–500 mesh). The 1000–500 μm and 250–125 μm size fractions were chosen to represent coarse and fine sand-size grains, respectively, and the 63–25 μm fraction was chosen to represent silt-size grains. Sample splits of each sieve size were then taken following the cone-and-quartering homogenization technique.<sup>47</sup> Sample splits were reserved for the supercritical CO<sub>2</sub> extractions and the following shale geochemical characterization analyses: (1) reflectance; (2) XRD; (3) BET surface area; and (4) SEM imaging. All size fractions and samples splits were stored in glass jars that were previously baked in a high-temperature muffle furnace (at 450 °C for 6 h) and sealed with polytetrafluoroethylene (Teflon)-lined lids until ready for analysis.

**Reflectance Analysis.** Reflectance analysis, performed in accordance with ASTM D7708<sup>48</sup> at the Organic Petrology Laboratory at the U.S. Geological Survey (USGS) in Reston, Virginia, was used to confirm the thermal maturity of the samples and to potentially identify the type of organic matter present. One sample from each core (3S-8, 2LT-12, and 4LG-3) was analyzed given the minor depth interval (<27 m) between samples within each core. Prior to analysis, the ground samples were mounted in a heat-setting thermoplastic to create pellets in a Buehler Simplicet 3000 Automatic Mounting Press, and subsequently polished with a Buehler Ecomet 4 according to ASTM D2797.<sup>49</sup> Reflectance measurements were made on a Leica DMRX incident light microscope equipped with a tungsten halogen discharge light source and a photomultiplier detector. Results were recorded as the percentage of incident white light reflected from the sample, %R<sub>w</sub>. Measurements were taken by using an oil immersion objective lens to increase microscope resolution, and calibrated against a glass standard (1.314 %R<sub>w</sub>). Average values were reported based on a total of 21–24 measurements for each sample with reported uncertainties within ±0.5 %R<sub>w</sub>. Quality assurance/quality control (QA/QC) was performed on a Hilgers microscope system with LED light source and digital camera detector.

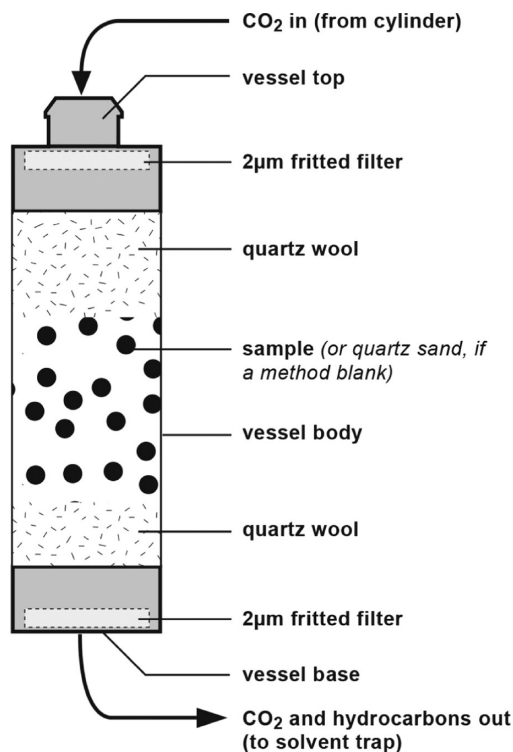
**X-ray Diffraction.** XRD was performed at the USGS in Reston, Virginia, to identify and quantify mineral constituents present within the samples. Prior to analysis, powdered shale samples (63–25 μm) were dried at 100 °C and then ashed at <100 °C.<sup>50</sup> Ashed samples were mounted as 25 mm pellets. XRD analyses were performed on a PANalytical X'Pert PRO X-ray diffractometer, where the sample pellets were irradiated with monochromatic Cu Kα X-radiation. Mineral phase identification and abundances were achieved by comparing the sample XRD patterns against a library of reference mineral standards.<sup>51,52</sup> Absolute uncertainties for measured mineral abundances are within ±1% (1σ).

**Supercritical Fluid Extractions.** Hydrocarbon extractions of all samples were performed on an ISCO SFX 220 supercritical fluid

extraction system coupled with an ISCO 260D model syringe pump at a USGS laboratory in Reston, Virginia. Borehole temperature data were not available for the shale samples used in this study, and thus, temperature and pressure conditions, 80 °C and 20.7 MPa (3000 psi), respectively, were chosen to represent approximate *in situ* reservoir conditions at sample depth (1920–2280 m), based upon a geothermal gradient of 30 °C/km (with an average surface temperature of 20 °C) and subsurface pressure gradient of 10.5 MPa/km (0.465 psi/ft).<sup>53</sup> At 80 °C and 20.7 MPa (3000 psi), the density of CO<sub>2</sub> is approximately 600 kg/m<sup>3</sup>.<sup>54,55</sup>

Extraction protocols were adapted from USGS Open-File Report 2006-1054.<sup>56</sup> Each extraction consisted of a 15 min static step, followed by a 1 hr dynamic step, with a corresponding flow rate of approximately 1.0–1.5 mL/min, whereby the total volume of CO<sub>2</sub> dispensed ranged between approximately 70 and 90 mL. A high restrictor (outlet line) temperature of 100 °C was chosen to minimize precipitation of heavy hydrocarbons or ice that could plug the line and reduce hydrocarbon recovery.<sup>14,15</sup> Temperature settings on the extractor were controlled by a Fuji electric sensor with a manufacturer accuracy of ±1 °C. The temperature sensor was calibrated using an alcohol thermometer, and the expected accuracy was confirmed. Pressure was also digitally controlled by the extractor, but was calibrated using an external NIST-certified pressure gauge (McMaster-Carr) to within a reported accuracy of ±3% (±0.69 MPa, 100 psi) of the target pressure (20.7 MPa, 3000 psi).

The extraction cell consisted of a 10 mL aluminum vessel with 2 μm opening frit filters inserted beneath the top and bottom vessel lids (Figure 2). A 1.0 g ground sample was added to the vessel, sandwiched



**Figure 2.** Aluminum vessel used in supercritical CO<sub>2</sub> extractions (10 mL capacity). Not drawn to scale. Modified from Kolak.<sup>56</sup>

between two small layers of quartz wool to minimize dead volume. The amount of O<sub>2</sub> in an empty vessel was estimated to be 2.1 mL. During extractions the vessel was approximately 90% filled with the sample and quartz wool; thus the O<sub>2</sub> content decreased by approximately 1 order of magnitude (2% of total cell volume).

Extracts were collected in 100 mL of chilled hexane (0 °C). Optimum temperature of the collection solvent, ranging between 0 and –5 °C, was found to minimize loss of volatile hydrocarbons, while

also preventing plugging of the restrictor line (which has been observed at very low temperatures of –40 °C).<sup>15</sup> Once extractions were terminated, bulk (unfractionated) extracts were subsequently concentrated to approximately 10 mL in a 125-mL pear flask using a vacuum rotary evaporator (Rotavap). Each extract was then transferred to a volumetric concentrator tube for evaporation to a final 5 mL volume using a nitrogen evaporator (N-EVAP). Each pear flask was rinsed three times with hexane, and all rinses added to the concentrator tube. Final 1:5 and 1:10 (extract:hexane) dilutions were necessary for the 3S sample extracts prior to analysis to prevent hydrocarbon peaks from saturating the GC-MS detector. Prior to analysis, 25 μL of a 1000 μg/mL perdeuterated internal standard solution was added to each 5 mL extract, containing *n*-dodecane-*d*<sub>26</sub> (*n*-C<sub>12</sub>D<sub>26</sub>), *n*-hexadecane-*d*<sub>34</sub> (*n*-C<sub>16</sub>D<sub>34</sub>), *n*-nonadecane-*d*<sub>40</sub> (*n*-C<sub>19</sub>D<sub>40</sub>), and *n*-triacontane-*d*<sub>62</sub> (*n*-C<sub>30</sub>D<sub>62</sub>) in equal amounts dissolved in hexane.

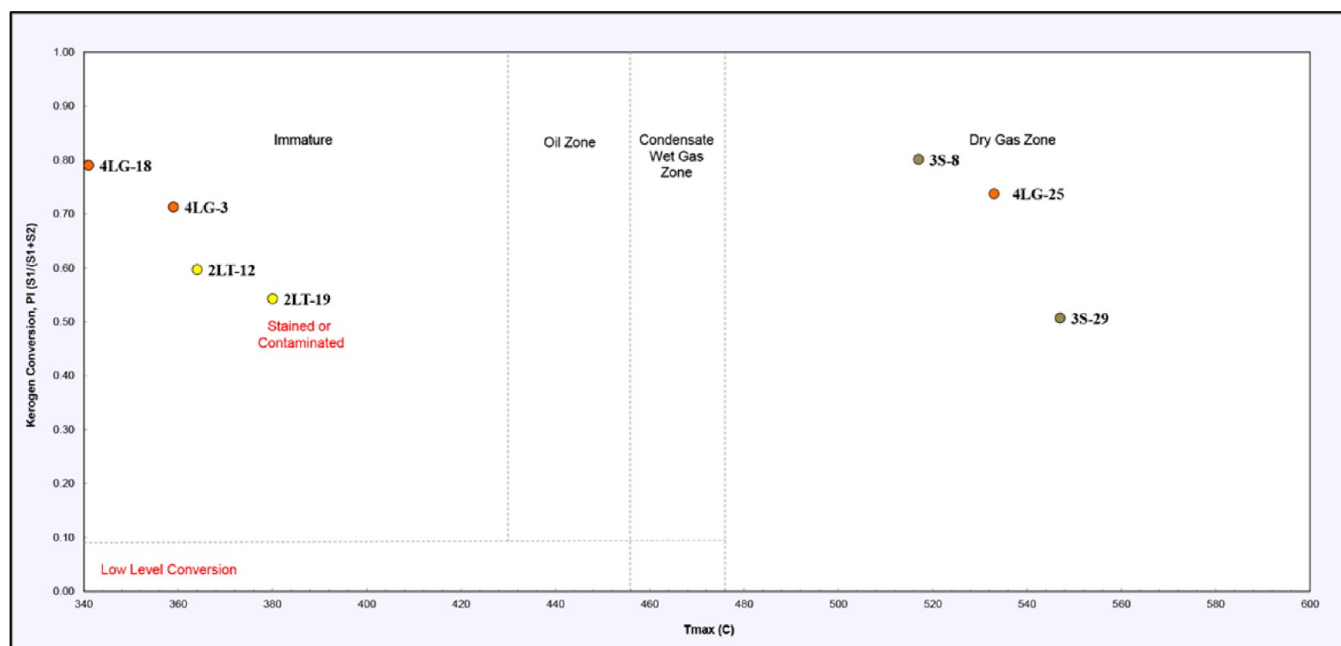
Triplicate extractions were performed on each sieve size for each sample as a measure of reproducibility. Quartz sand, previously baked in a muffle furnace at 450 °C for 6 h, was used as a method blank at the start of each batch of extractions (daily) to monitor for contamination. Each sample and method blank was spiked with a perdeuterated surrogate solution containing *n*-decane-*d*<sub>22</sub> (*n*-C<sub>10</sub>D<sub>22</sub>) and *n*-tetracosane-*d*<sub>50</sub> (*n*-C<sub>24</sub>D<sub>50</sub>) in hexane, just prior to the start of each extraction to estimate extraction efficiency. The *n*-C<sub>10</sub>D<sub>22</sub> surrogate was chosen to monitor recovery of lower molecular weight, volatile hydrocarbons, while *n*-C<sub>24</sub>D<sub>50</sub> was chosen to monitor recovery of higher molecular weight, low-volatility hydrocarbons.

Additional method validation extractions included a time study wherein the length of the dynamic step was evaluated over 0.5, 1, 2, and 3 h time segments.

This study used “Bone Dry” (99.9% minimum purity) CO<sub>2</sub> contained in a high-pressure cylinder equipped with a siphon (Airgas, Inc.). Nitrogen gas (HP grade) for the N-EVAP was also purchased from Airgas, Inc. All perdeuterated hydrocarbon surrogate and internal standards were purchased from Sigma-Aldrich, Inc., with stock solutions prepared in *n*-hexane (TraceSELECT, Sigma-Aldrich, Inc.). Quartz sand used for all method blanks was also purchased from Sigma-Aldrich, Inc.

**Gas Chromatography–Mass Spectrometry Analysis.** Quantitative analysis of total resolvable *n*-aliphatic hydrocarbons from all extracts was performed on an Agilent 6890 series gas chromatograph (GC) interfaced with an Agilent 5973 mass-selective detector (MSD). Automatic sample injection was performed with an Agilent 7683 Series Automatic Injector, operating in splitless mode to maximize resolution of trace compounds. The instrument was equipped with an HP-5MS capillary column (30 m × 0.25 mm × 0.25 μm). Operating conditions included (1) a 1 μL injection volume; (2) 0.9 mL/min carrier gas (He) flow rate; and (3) 50 °C initial oven temperature (holding for 1.5 min), followed by an oven temperature ramp to 315 °C at 10 °C/min, followed by a 15 min hold time at 315 °C.<sup>56</sup> The MSD operated in full-scan mode (35–500 amu). Target hydrocarbon peaks were identified by their GC retention times and mass spectral fragmentation patterns in comparison to standard compounds. Quantitative measurements were made from the signal intensity (total ion counts/second) for the area under the peak of the user-defined target ion (base peak, *m/z* = 57). An external seven-point calibration curve (0.25–10.0 μg/mL) was generated for an *n*-aliphatic hydrocarbon standard solution (*n*-C<sub>9</sub> through *n*-C<sub>40</sub> in hexane), and a six-point calibration curve was generated for the surrogate standard solution (*n*-C<sub>10</sub>D<sub>22</sub> and *n*-C<sub>24</sub>D<sub>50</sub> in hexane). A quadratic regression model was used to establish the best fit relationship between concentration and response, with coefficient of determination (*r*<sup>2</sup>) values ≥0.999 for *n*-C<sub>9</sub> through *n*-C<sub>30</sub>. Calibration was checked with each batch of sample extracts. Helium (BIP grade) was purchased from Airgas, Inc. The *n*-C<sub>7</sub> through *n*-C<sub>40</sub> saturated alkane mixture used for calibration was purchased from Sigma-Aldrich, Inc., with stock solutions prepared in *n*-hexane (TraceSELECT, Sigma-Aldrich, Inc.).

**Brunauer–Emmett–Teller Surface Area Analysis.** Specific surface area was measured on a subset of ground samples to evaluate differences in surface area among the sieve size fractions. One sample



**Figure 3.** Kerogen conversion and maturity plot derived from Rock-Eval II pyrolysis data, relating production index (PI) to  $T_{\max}$  values. Analyses performed by GeoMark Research, Ltd.

from each core (3S-8, 2LT-12, and 4LG-3) was analyzed (all sieve size fractions). Surface area analyses were performed by Particle Technology Labs on a Micromeritics TriStar II 3020 static pressure (volumetric) analyzer, with  $N_2$  as the adsorbate gas. Accuracy for the BET surface area results is within  $\pm 0.24 \text{ m}^2/\text{g}$  ( $\pm 1\%$ ), which is within the range of accepted instrumental accuracy of  $\pm 3.45\%$  (at the 99.7% confidence level). Uncertainties, determined from triplicate analyses, have been reported to within  $\pm 0.3 \text{ m}^2/\text{g}$  ( $\pm 1\%$ ,  $\pm 1$  standard error of the mean,  $\sigma_m$ ).

**Scanning Electron Microscopy.** SEM imaging was performed on a JEOL 8900 Electron Probe Microanalyzer at the University of Maryland to visualize and characterize the surface of sample particles within each sieve size fraction. Prior to analysis, samples were mounted on carbon tape and then coated with a thin layer of carbon fibers to minimize charging at the surface. Both secondary electron (SE) and back-scatter electron (BSE) images were taken of the 1000–500  $\mu\text{m}$  and 250–125  $\mu\text{m}$  sieve size fractions of sample 4LG-3.

Additional high-resolution SE images of shale pore structure were taken with a JEOL 5800-LV field emission scanning electron microscope (FESEM) at the USGS Denver Microbeam Laboratory. Prior to analysis, sample chips (one from each core) were polished, ion-milled, and carbon-coated using a carbon evaporator.

## RESULTS

**Rock-Eval II Pyrolysis and TOC Analysis.** Rock-Eval II pyrolysis was used as an initial screening technique to evaluate the quantity, quality, and thermal maturity of organic matter in 31 shale samples. Quantity of organic matter, or organic richness, was evaluated based upon TOC content, which is composed of the pyrolyzable carbon fraction (S1 and S2) and the residual carbon fraction.<sup>45</sup> The S1 and S1/TOC parameters were the key criteria used to screen samples for subsequent solvent extractions. Although S1 does not correspond directly to solvent-extracted organic matter,<sup>31,45</sup> this parameter is a crude approximation of potentially extractable hydrocarbon content. The seven samples selected for the supercritical  $\text{CO}_2$  extractions had the highest S1 and S1/TOC values of the initial sample set (Table 1).

Very low hydrogen index ( $\text{HI} \equiv \text{S}_2/\text{TOC}$ ) values ( $< 50 \text{ mg HC/g TOC}$ ) and oxygen index ( $\text{OI} \equiv \text{S}_3/\text{TOC}$ ) values ( $< 39 \text{ mg CO}_2/\text{g TOC}$ ) were found for all samples. A modified Van Krevelen diagram suggests that the type of kerogen present could be oxidized, highly mature, or Type IV kerogen.<sup>45,57</sup> However, low HI (0–100) and OI (5–30) values of other Devonian shales in the Appalachian Basin are suggested to represent original Type II organic matter converted to Type IV (inert solid bitumen) by a high degree of thermal maturation.<sup>58</sup>

Thermal maturity, which can be roughly estimated from  $T_{\max}$  and production index ( $\text{PI} \equiv \text{S}_1/(\text{S}_1+\text{S}_2)$ ) measurements, indicates the degree to which kerogen is transformed into free hydrocarbons.<sup>45,46</sup> Sample PI values range from 0.5 to 0.8, which suggests they are in a late-mature/post-mature stage of hydrocarbon generation, the dry gas window, occurring at subsurface paleotemperatures of approximately 150–200  $^\circ\text{C}$ .<sup>45</sup> Yet,  $T_{\max}$  values for the 2LT core samples (2LT-12 and 2LT-19) and two out of three of the 4LG core samples (4LG-3 and 4LG-18) are suggestive of immature sediments, which is not in agreement with associated PI values for those samples. A kerogen conversion and maturity plot (Figure 3) suggests that those samples are potentially “stained or contaminated”, whereas the three other samples plot within the dry gas zone (3S-8, 3S-29, and 4LG-25). Sample pyrograms, however, are not characteristic of contaminated reservoir rocks, either by oil-based or water-based additives, lubricants, or natural, migrated oil.<sup>45</sup> There is also no distinctive feature of the pyrograms distinguishing two groups of samples (dry gas zone versus stained/contaminated). Thus, although possible contamination cannot be ruled out for the samples in this study, the low S1 and S2 peak values, and low derived HI, suggest that the likelihood of contamination is low. Furthermore, given the low S2 peaks, S2 and  $T_{\max}$  values are often inaccurate, as are derived Rock-Eval parameters (i.e., PI and HI), and should be supported by additional geochemical analyses.<sup>45</sup>

**Organic Petrography.** Reflectance measurements of the observable organic matter, ranging from 2.2 to 2.6 ( $\pm 0.5$ ) % $R_o$ ,



Table 2. Reflectance Analysis Measurements of Solid Bitumen (Pyrobitumen)

sample ID	no. of measurements	mean (%R <sub>o</sub> )	uncertainty <sup>a</sup> (±%R <sub>o</sub> )	relative uncertainty (%)
3S-8	24	2.3	0.3	15
2LT-12	21	2.6	0.5	18
4LG-3	23	2.2	0.4	17

<sup>a</sup>Uncertainties are reported as  $\pm 1\sigma$ .

(Table 2), confirm a high degree of thermal maturity for the shale samples (dry gas window). These reflectance values are slightly higher than those reported on regional thermal maturity maps (approximately 1.3–2 %R<sub>o</sub>) for Appalachian Basin Devonian shales in the counties wherein these cores were drilled.<sup>44,58,59</sup> However, given the uncertainties for these measurements, there is no significant difference among thermal maturity values. Thermal maturity zones reported across the Appalachian Basin are also compiled from both reflectance (% R<sub>o</sub>) and conodont color alteration index (CAI) measurements taken on different samples within the basin, and currently there is no conversion factor between the two indices.<sup>44</sup>

Reflectance measurements also reveal the predominant form of organic matter to be solid pyrobitumen, as evidenced by its pore-lining and pore-filling texture, and growth around mineral grains (Figure 4).<sup>60,61</sup> The principal type of original organic

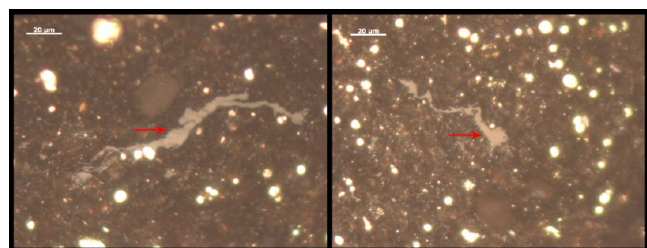


Figure 4. Reflectance images of pyrobitumen. Red arrows point to pyrobitumen within the shale matrix. Bright framboidal pyrite structures are dispersed throughout. Left: 3S-8, with a reflectance value of 2.6 %R<sub>o</sub>. Right: 2LT-12, with a reflectance value of 3.0 %R<sub>o</sub>.

matter, Type II kerogen (*Tasmanites* algae, a telalginite maceral, and bituminite macerals), was inferred from studies of other low-maturity Marcellus Shale and Devonian-age shales elsewhere in the Appalachian Basin.<sup>58,62</sup>

**XRD.** The XRD results show that all samples are composed of primarily quartz (24–40%) and clay (mainly illite) minerals (12–62%) (Figure 5, Tables 3 and 4). Carbonate minerals are only abundant in samples 3S-29 (46%) and 4LG-18 (36%). Minor mineral constituents (<10% and  $\geq 5\%$ ) include pyrite and chlorite. Feldspars are present in trace quantities (<5%). The mineralogy is similar to that reported for other Marcellus Shale samples.<sup>25,62–64</sup>

**Supercritical CO<sub>2</sub> Extractions: Distribution of Extracted Hydrocarbons.** Supercritical CO<sub>2</sub> extracted *n*-aliphatic hydrocarbons in the range of predominantly *n*-C<sub>11</sub> through *n*-C<sub>21</sub>, with highest recovery between *n*-C<sub>12</sub> and *n*-C<sub>15</sub>. No significant difference is observed in the distribution of extracted *n*-aliphatic hydrocarbons between sieve size fractions for a given sample, or between samples within a given core. However, a few distinctions are noticeable among cores (Figure 6). Only hydrocarbons *n*-C<sub>11</sub> through *n*-C<sub>14</sub> are present in the 3S sample extracts. The 2LT and 4LG sample extract chromatograms reveal additional compounds, including branched aliphatic hydrocarbons. All 4LG sample extracts

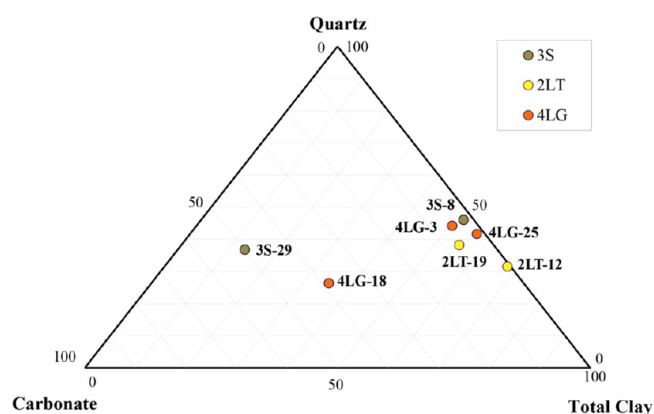


Figure 5. Ternary diagram showing the relative proportions of total clay, carbonate and quartz in each sample.

contain *n*-aliphatic hydrocarbons ranging from approximately *n*-C<sub>11</sub> through *n*-C<sub>21</sub>. The 2LT sample extracts have a tighter distribution range of resolvable *n*-aliphatic hydrocarbons (*n*-C<sub>11</sub> through *n*-C<sub>14</sub>), yet a broad unresolved complex mixture (UCM) is also evident with qualitatively identifiable *n*-aliphatic peaks ranging from approximately *n*-C<sub>18</sub> through *n*-C<sub>23</sub>. The source and chemical composition of the UCM is unknown, but previous work suggests the UCM may result from petroleum compounds resistant to chemical and biological degradation, or from different sources of petroleum contamination.<sup>65</sup> However, the Rock-Eval II data (Table 1) and pyrograms discussed above provide supporting evidence that the likelihood of contamination (by drilling additives or natural, non-indigenous hydrocarbons) is low.

**Supercritical CO<sub>2</sub> Extractions: Quantity of Extracted Hydrocarbons.** The quantity of extracted total resolvable, *n*-aliphatic hydrocarbons ranges from approximately 0.01 to 0.6 parts per thousand by weight (mg HC/g rock), or 0.3–12 (mg HC/g TOC). Results indicate an order of magnitude increase in yield from the 3S extracts (all sieve size fractions), in comparison to that recovered from the 2LT and 4LG extracts (Figure 7). Extraction results also reveal a trend among all samples with regard to sieve size, showing a slight increase in hydrocarbon yield from the intermediate (250–125  $\mu$ m) sieve size fraction, followed by a drop in yield from the 63–25  $\mu$ m sieve size fraction.

Relative uncertainty, i.e., the ratio of the standard error of the mean ( $\sigma_m$ ) to the average, expressed as a percent, was used to evaluate precision. Measurement uncertainties range between  $\pm 2$  and 11% for each set of triplicate extractions performed on each sieve size fraction for a given sample. For most of the extractions, *n*-C<sub>11</sub> through *n*-C<sub>13</sub> have the highest deviation and contribute the largest source of error to the overall results. Slight fluctuations in the volume of CO<sub>2</sub> dispensed in each extraction (70–90 mL) among replicate extractions may have also contributed a source of variability. Surrogate standard recovery totals, averaged across all extractions (samples and method blanks), are  $47 \pm 3\%$  for *n*-C<sub>10</sub>D<sub>22</sub> and  $97 \pm 2\%$  for *n*-

Table 3. Nomenclature for XRD Results

label	mineral name(s)	mineral formula(s)
QTZ	quartz	SiO <sub>2</sub>
FLD	K-feldspar and Plagioclase (albite to anorthite)	KAlSi <sub>3</sub> O <sub>8</sub> and NaAlSi <sub>3</sub> O <sub>8</sub> (albite) to CaAl <sub>2</sub> Si <sub>2</sub> O <sub>8</sub> (anorthite)
CARB	calcite, ankerite, dolomite, and siderite	CaCO <sub>3</sub> , Ca(Fe <sup>2+</sup> ,Mg)(CO <sub>3</sub> ) <sub>2</sub> , CaMg(CO <sub>3</sub> ) <sub>2</sub> , and FeCO <sub>3</sub>
I/S	illite/smectite	K <sub>y</sub> Al <sub>4</sub> (Si <sub>8-y</sub> ,Al <sub>y</sub> )O <sub>20</sub> (OH) <sub>4</sub> (1 < y < 1.5)/(1/2Ca,Na)(Al,Mg,Fe) <sub>4</sub> (Si <sub>4</sub> Al <sub>8</sub> O <sub>20</sub> (OH) <sub>4</sub> ·nH <sub>2</sub> O)
KAOL	kaolinite	Al <sub>2</sub> Si <sub>2</sub> O <sub>5</sub> (OH) <sub>4</sub>
CHLR	chlorite	Mg <sub>2</sub> Al <sub>2</sub> SiO <sub>5</sub> (OH) <sub>4</sub>
PY	pyrite, marcasite, and sphalerite	FeS <sub>2</sub> , FeS <sub>2</sub> , and (Zn,Fe)S
other	trace (low-level qualitative ID)	N/A

Table 4. Major ( $\geq 50\%$ ), Minor ( $<10\%$  and  $\geq 5\%$ ), and Trace ( $<5\%$ ) Phase Mineralogy

sample ID	QTZ	FLD	CARB	I/S	I	KAOL	CHLR	PY	other	total clay
3S-8	40.4	1.8	1.8	0.0	37.0	0.0	8.5	9.6	0.8	45.5
3S-29	34.1	1.5	46.3	0.0	12.3	0.0	0.0	4.3	0.0	12.3
2LT-12	28.9	1.9	0.6	0.0	51.3	0.0	10.8	6.0	0.0	62.1
2LT-19	33.0	2.2	5.9	0.0	45.4	0.0	2.0	9.7	0.3	47.4
4LG-3	39.7	2.7	4.7	0.0	36.0	0.0	9.4	7.1	0.0	45.4
4LG-18	24.4	0.7	35.7	0.0	27.7	0.0	4.8	5.8	0.0	32.5
4LG-25	36.1	2.4	1.4	0.0	43.1	0.0	6.0	9.8	0.6	49.1
uncertainty <sup>a</sup> ( $\pm\%$ )	0.7	0.5	0.2	0.0	0.4	0.0	0.5	0.8	0.1	0.7

<sup>a</sup>Uncertainties are reported within  $\pm 1\sigma$ .

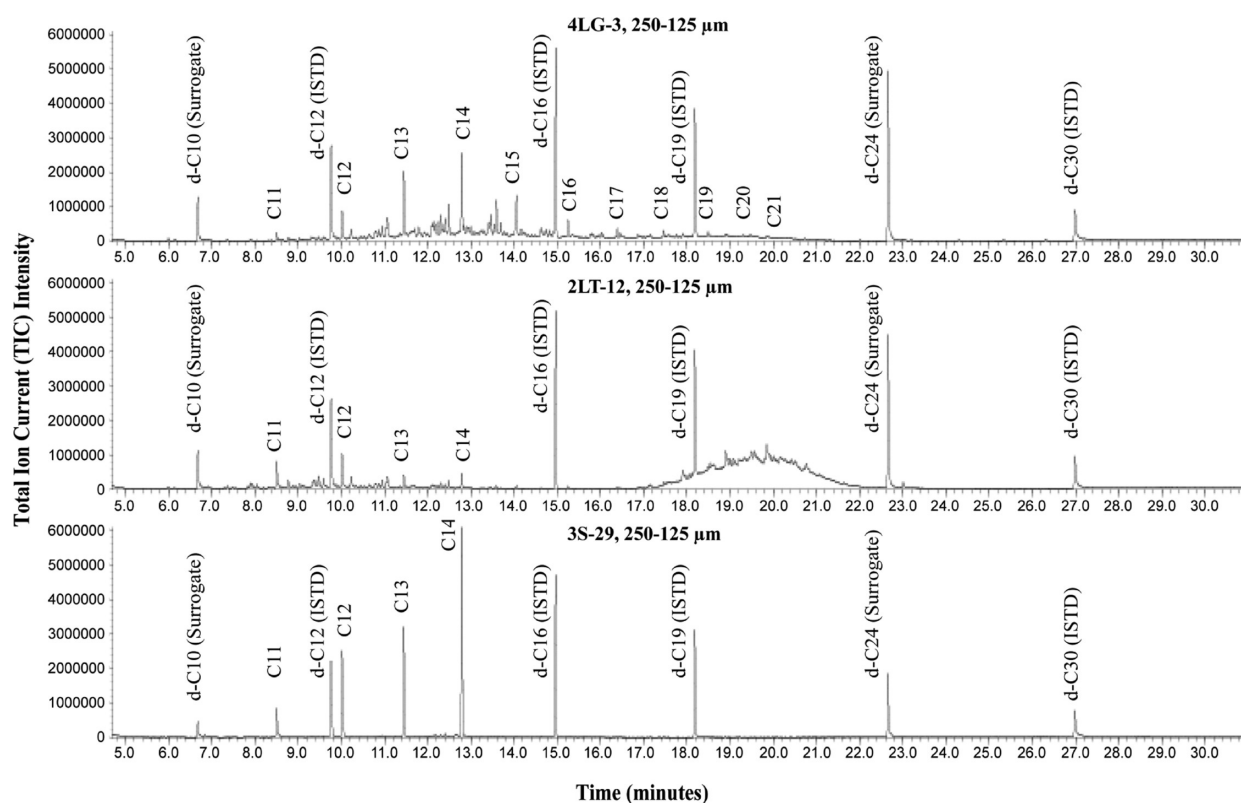
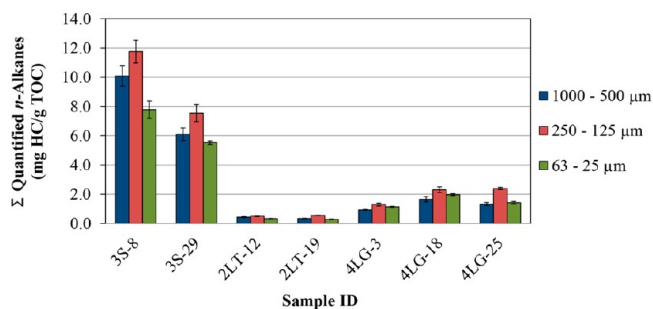


Figure 6. Total ion current chromatograms of representative samples from each core. Chromatograms highlight the difference in distribution of extracted *n*-aliphatic hydrocarbons between cores.

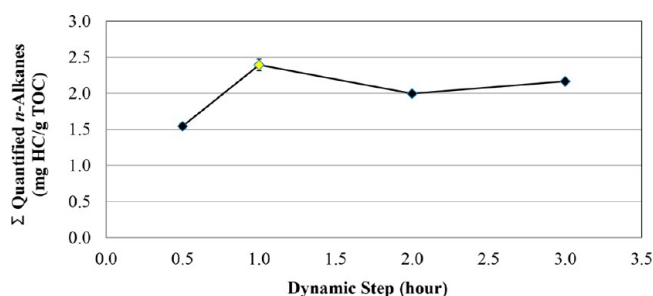
C<sub>24</sub>D<sub>50</sub>. Uncertainties for surrogate standards are reported as  $\pm 1\sigma_m$ . Higher volatility of the lower molecular weight surrogate (*n*-C<sub>10</sub>D<sub>22</sub>), and of target hydrocarbons of similar molecular weight, may make them more sensitive to loss in postextraction (solvent evaporation) steps in this extraction method, accounting for lower-than-expected yields.<sup>21,66</sup>

To examine whether extraction time had an effect on the quantity or distribution of extracted hydrocarbons, a series of

extractions were performed wherein the time of the dynamic step was changed from 1 h to 30 min, 2 h, and 3 h increments. Sample splits from the 4LG-25, 250–125  $\mu\text{m}$  fraction were used in each extraction. Results (Figure 8, Table 5) identify highest recovery from the 1 h dynamic step, wherein the average volume of CO<sub>2</sub> dispensed in the triplicate extractions is approximately 86 mL. The 30 min dynamic step yielded the lowest recovery. Results suggest that extraction yield is



**Figure 7.** Supercritical CO<sub>2</sub> extractions: Total quantity of resolvable *n*-aliphatic hydrocarbons extracted from each sample as a function of sieve size. Error bars are  $\pm 1\sigma_m$ .



**Figure 8.** Relationship between extraction time and hydrocarbon yield for the supercritical CO<sub>2</sub> extractions. The length of the dynamic (flow through) step was varied for sample 4LG-2S, 250–125 μm sieve size. The reported value for the 1 h extraction is an average value from triplicate extractions with an uncertainty of  $\pm 0.1$  mg HC/g TOC ( $\pm 1\sigma_m$ ). Only one extraction was performed for the 30 min, 2 h, and 3 h extractions. Results show a 43% increase in hydrocarbon yield by increasing the length of time for the dynamic step from 30 min to 1 h. A decrease in yield was then observed as the dynamic step was extended to 2 h and 3 h intervals (18% and 10% decline in yield, relative to the 1 h interval, respectively).

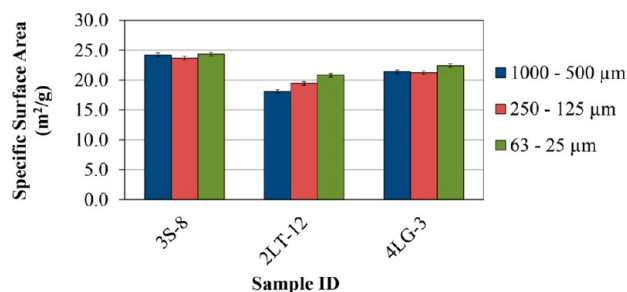
**Table 5. Percent Difference in Extraction Yield as a Function of Time**

dynamic step duration (h)	total quantified <i>n</i> -alkanes (mg HC/g TOC)
0.5	1.5
1	2.4
2	2.0
3	2.2

optimized with the 1 h dynamic step used in our supercritical CO<sub>2</sub> extractions.

**Surface Area Analysis and SEM Imaging.** Surface area results do not reveal any significant variation nor consistent trend among sieve sizes (Figure 9, Table 6). However, subsequent SEM images reveal that individual crushed shale particles within each sieve size fraction are coated in a layer of smaller adhered fine particles (Figures 10 and 11). Thus, the sieve size fractions used in this study are merely sieve size ranges and not a true indication of rock matrix grain size distribution.

Additional FESEM images (Figure 12) reveal a mixed-pore network for each sample (3S-8, 2LT-12, and 4LG-3), including nanometer-size pores associated with both the organic matter and the mineral matrix (interparticle and intraparticle) using Loucks et al.'s<sup>26</sup> pore type classification for mudrocks. Pores present within the organic matter are heterogeneous in distribution and shape, ranging from simple spheroid and

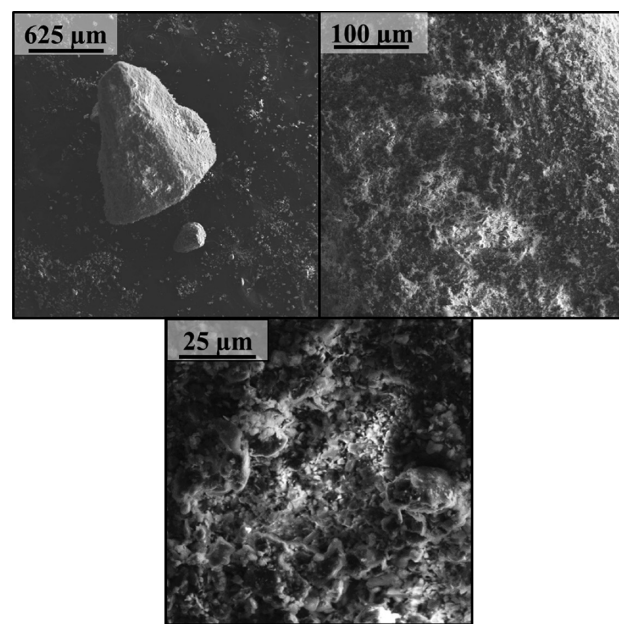


**Figure 9.** Specific surface area results. Results from each sample are reported as a function of sieve size. Error bars are  $\pm 1\sigma_m$ .

**Table 6. BET Specific Surface Area Results**

sample ID	sieve size (μm)	specific surface area (m <sup>2</sup> /g)	uncertainty <sup>a</sup> (±m <sup>2</sup> /g)	relative uncertainty (%)
3S-8	1000–500	24.2	0.3	1
	250–125	23.7	0.3	1
	63–25	24.3	0.3	1
2LT-12	1000–500	18.1	0.3	2
	250–125	19.5	0.3	2
	63–25	20.8	0.3	1
4LG-3	1000–500	21.4	0.3	1
	250–125	21.2	0.3	1
	63–25	22.4	0.3	1

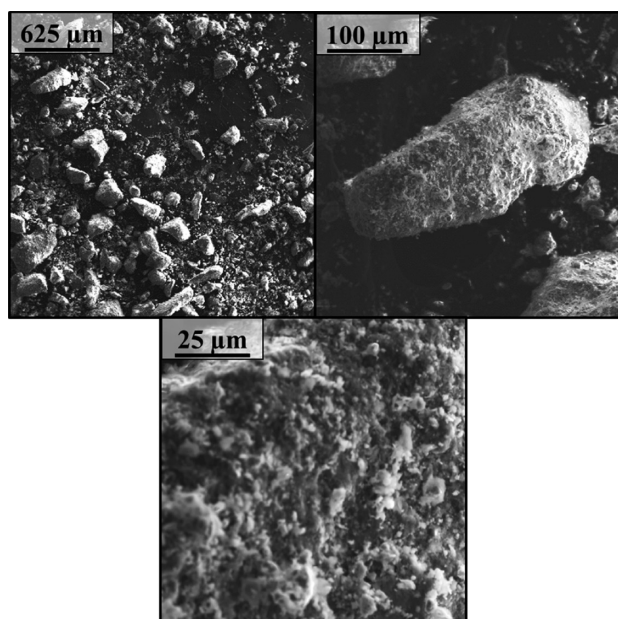
<sup>a</sup>Reported uncertainties are  $\pm 1\sigma_m$ .



**Figure 10.** SEM images of 4LG-3, 1000–500 μm sieve size fraction. Magnification: top left, 40×; top right, 250×; and bottom, 1000×.

elliptical structures to more complex, irregular shapes. The interparticle pores (intergranular and intercrystalline) have no visible preferred orientation, with a variety of shapes ranging from elongated, elliptical pores to triangular and more complex, irregular void spaces. Intraparticle pores are visible as intercrystalline pores within pyrite framboids (Figure 12,





**Figure 11.** SEM images of 4LG-3, 250–125  $\mu\text{m}$  sieve size fraction. Magnification: top left, 40 $\times$ ; top right, 250 $\times$ ; and bottom, 1000 $\times$ .

bottom right), dissolution pores around the rim of an unidentified mineral (Figure 12, bottom right), and within aggregates of clay grains (Figure 12, bottom left).

## DISCUSSION

**Extracted Hydrocarbons.** The total yield of extracted *n*-aliphatic hydrocarbons ranges from approximately 0.3 to 12 mg HC/g TOC, with lowest recovery from the 2LT samples and highest recovery from the 3S samples. The overall distribution of extracted *n*-aliphatic hydrocarbons ranges from predominantly *n*-C<sub>11</sub> through *n*-C<sub>21</sub>, with highest yields between *n*-C<sub>12</sub> and *n*-C<sub>15</sub>. A greater proportion of aliphatic hydrocarbons with carbon number < C<sub>19</sub> are generated from high-maturity samples, relative to heavier C<sub>19+</sub> hydrocarbons typically associated with thermally immature samples, likely due to an increase in the degree of thermal degradation of organic matter associated with advanced levels of maturity.<sup>58</sup> The distribution of hydrocarbons recovered in this study is also comparable to previous supercritical CO<sub>2</sub> extraction studies wherein organic matter was extracted from petroleum source rocks under similar extraction conditions.<sup>14,15,18</sup>

No apparent differences are observed among cores with regard to organic matter content, mineralogy, or surface area and pore imaging analyses that could account for the discrepancies in the quantity or distribution of extracted hydrocarbons. The Rock-Eval II data (Table 1) and pyrograms also support the interpretation that the likelihood of contamination in these samples is low. Thus, the extracted hydrocarbons most likely reflect naturally occurring, residual organic matter present within the shale matrix.

Lower yields observed in the supercritical CO<sub>2</sub> extractions compared to S1 (and S1/TOC) values measured via Rock-Eval II pyrolysis (Table 1) are expected given sample preparation and procedural differences between the two extraction techniques. Solvent extractions typically cause greater loss of lower molecular weight, more volatile hydrocarbons, relative to pyrolysis, largely due to solvent evaporation prior to analysis. Solvent-extracted organic matter is also dependent upon

solvent polarity and extraction parameters.<sup>45,67</sup> Additionally, only the resolvable *n*-aliphatic hydrocarbons, a fraction of the bulk extract, were quantified in our supercritical CO<sub>2</sub> extractions.

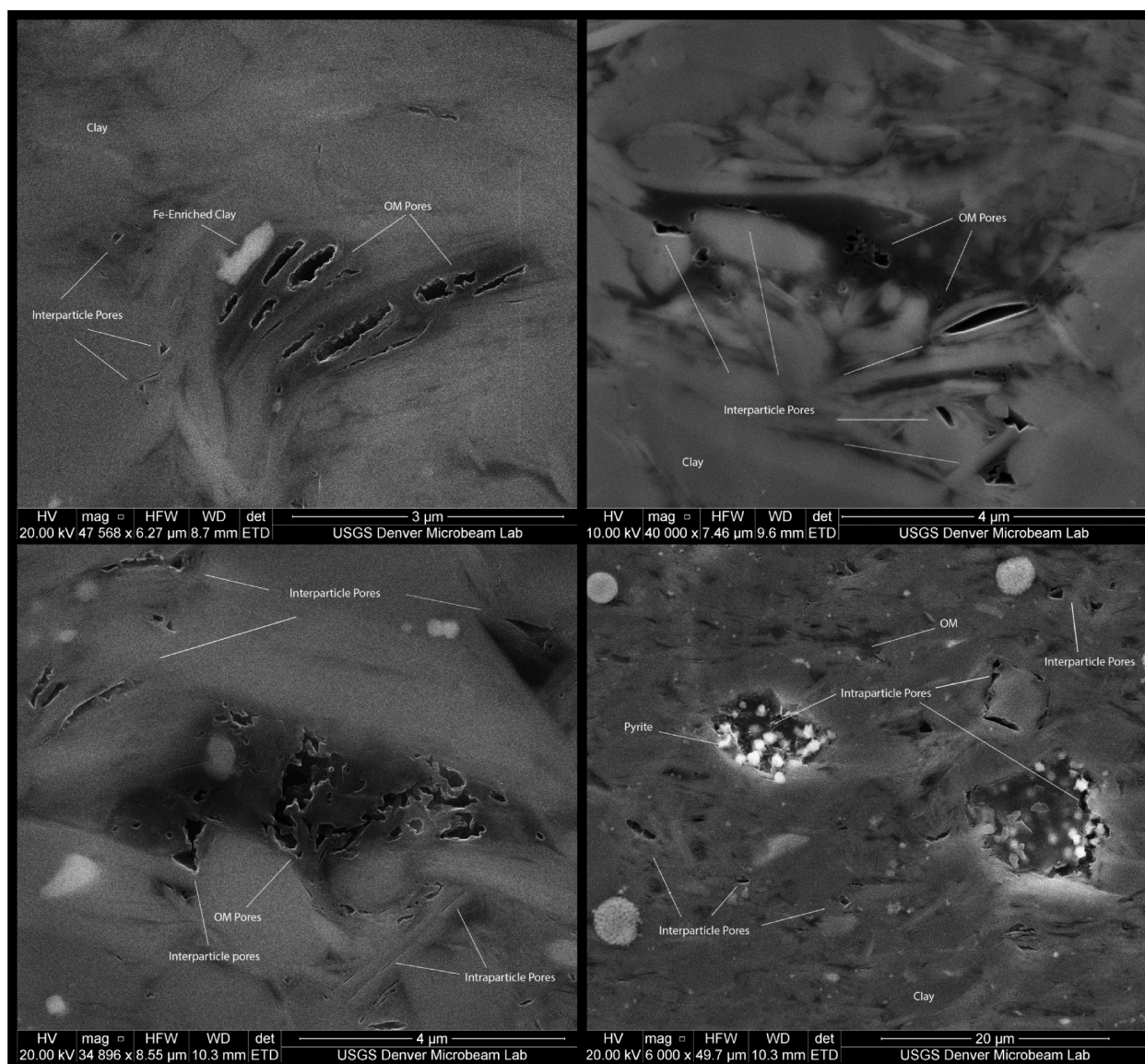
No strong correlation was established between hydrocarbon yield and sieve size. However, a trend is observed in all sample extracts, with highest recovery from the 250–125  $\mu\text{m}$  sieve size fraction. The effect of sieve size on extraction yield may not be as significant as was initially expected. Lack of a significant relationship could have been obscured by the coating of adhered fine particles discovered on all individual crushed shale particles (Figures 10 and 11), suggesting an overlap of rock matrix grain sizes across the sieve size fractions. Further considerations include loss of volatile compounds upon crushing the shale, and potential channeling and particle aggregation effects, especially within the 63–25  $\mu\text{m}$  fraction, all of which could have reduced extraction rates and overall recovery.<sup>20,35,36,38</sup>

Additional steric limitations may also have a substantial effect on hydrocarbon yield among particle sizes. The Marcellus and other Devonian shales have pore and pore throat sizes on the order of 10<sup>-1</sup>–10<sup>-3</sup>  $\mu\text{m}$  in diameter.<sup>24,25</sup> Thus, with an effective molecular diameter of 3.3 Å (3.3  $\times$  10<sup>-4</sup>  $\mu\text{m}$ ),<sup>22</sup> CO<sub>2</sub> can access nanometer-size pores of shale matrices. However, some petroleum hydrocarbon constituents can have molecular diameters (roughly 5–50 Å for asphaltene molecules/aggregates down to 3.8 Å for methane)<sup>22,24,68</sup> of approximately the same order of magnitude as characteristic shale pore and pore throat sizes, 10<sup>-2</sup>–10<sup>-4</sup>  $\mu\text{m}$ .<sup>22,24–26</sup> Thus, although CO<sub>2</sub> can access particle surface porosity and solvate potentially extractable hydrocarbons, the resultant supercritical fluid mixture may not be able to effectively navigate through/out of the shale porosity network. If this is the case, a threshold of hydrocarbon extraction may have been reached, contributing to a lack of trend among sieve size fractions.

**Effect of Surface Area and Porosity.** No clear inverse relationship was observed between surface area and particle size for this sample set. One potential factor contributing to the lack of significant variation of surface area among the designated sieve size ranges is the coating of adhered fine particles found on all individual crushed shale particles, as discussed above (Figures 10 and 11).

Another potential explanation is that different techniques for characterizing surface area and porosity (i.e., low-pressure N<sub>2</sub> and CO<sub>2</sub> gas adsorption, mercury intrusion, helium porosimetry, and small-angle neutron scattering/ultra-small-angle neutron scattering (SANS/USANS) techniques can yield different results. Varying results of gas adsorption techniques in particular may reflect the size and shape of both the adsorbate gas molecules and pores of the adsorbent surface, accessibility of the adsorbing gas to the pores, and molecular interactions between the gas and sample surface.<sup>27,28,69,70</sup>

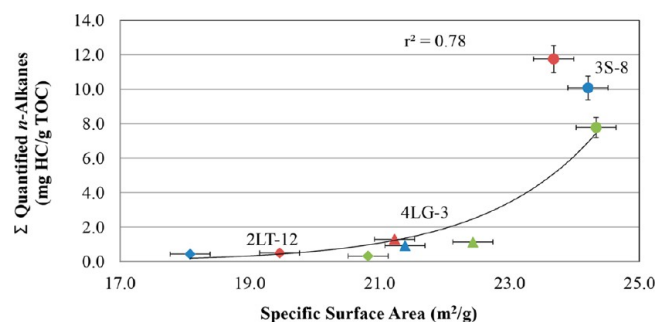
Nitrogen, with a molecular cross-sectional area of 0.162 nm<sup>2</sup> (at 77 K) is considered a widely suitable adsorptive gas for measuring surface area, resulting in BET surface areas within 20% of true surface areas.<sup>69</sup> However, at 77 K (–196 °C), N<sub>2</sub> has insufficient thermal energy to diffuse through narrow pore networks. Alternatively, CO<sub>2</sub> (0.251 nm<sup>2</sup> molecular cross-sectional area), used in adsorption analyses at a higher temperature (273 K, 0 °C), has the necessary thermal energy to access a microporous adsorbent.<sup>71</sup> Whereas both N<sub>2</sub> and CO<sub>2</sub> can access mesopores (2–50 nm) of shale and coal matrices, micropores (<2 nm) are more accessible to CO<sub>2</sub>.<sup>28</sup>



**Figure 12.** SEM images taken from the FESEM analysis of pore structure: top left, 3S-8; top right, 4LG-3; bottom left, 2LT-12; and bottom right, 2LT-12.

Consequently, surface areas measured with  $\text{CO}_2$  are often 1–2 orders of magnitude larger than those measured with  $\text{N}_2$ .<sup>71</sup> A comparison of these adsorption methods on mature shale and other source rocks likewise show an increase in specific surface area when measured with  $\text{CO}_2$ , depending upon the abundance of micropores associated with organic matter.<sup>27–29</sup> Thus, the use of  $\text{N}_2$  to measure surface area in this study may be obscuring a potential trend of exposed surface area with particle size. Accordingly, supercritical  $\text{CO}_2$  may be accessing and extracting hydrocarbons from pores not detected by  $\text{N}_2$ -derived surface area measurements or SEM imaging, subsequently obscuring a more accurate relationship of extraction yield as a function of surface area, regardless of sieve size range (Figure 13).

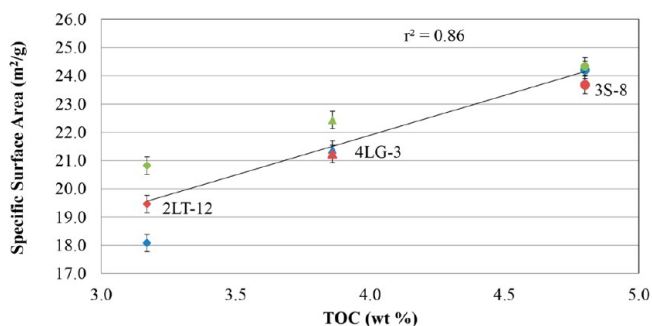
Nevertheless, a plot of surface area as a function of TOC content (Figure 14) shows a positive correlation between the two variables. Previous studies have also found positive correlations between both mesoporosity and microporosity (surface areas and volumes) and TOC content in shales, suggesting that porosity within organic matter is signifi-



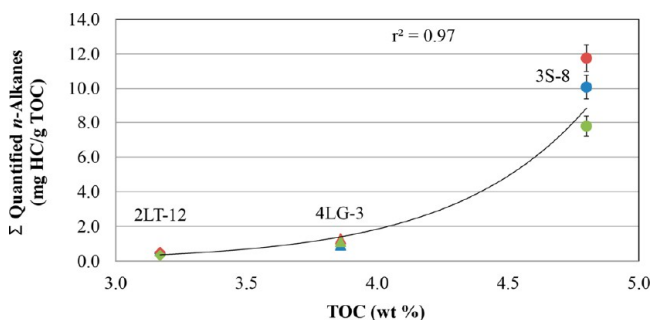
**Figure 13.** Extraction yield as a function of specific surface area. Vertical and horizontal error bars are  $\pm 1\sigma_m$ . Samples: 3S-8 (circles), 4LG-3 (triangles), 2LT-12 (diamonds). Sieve ranges: 1000–500  $\mu\text{m}$  (blue), 250–125  $\mu\text{m}$  (red), and 63–25  $\mu\text{m}$  (green).

cant.<sup>27–29,72–74</sup> Given that extraction yield also increases with increasing TOC content (Figure 15), the exposed internal surface area of pores associated with organic matter may be an important controlling factor on extraction yield.





**Figure 14.** Specific surface area as a function of TOC. Vertical error bars are  $\pm 1\sigma_m$ . Samples: 3S-8 (circles), 4LG-3 (triangles), 2LT-12 (diamonds). Sieve ranges: 1000–500  $\mu\text{m}$  (blue), 250–125  $\mu\text{m}$  (red), and 63–25  $\mu\text{m}$  (green).



**Figure 15.** Extraction yield as a function of TOC. Vertical error bars are  $\pm 1\sigma_m$ . Samples: 3S-8 (circles), 4LG-3 (triangles), 2LT-12 (diamonds). Sieve ranges: 1000–500  $\mu\text{m}$  (blue), 250–125  $\mu\text{m}$  (red), and 63–25  $\mu\text{m}$  (green).

## CONCLUSIONS

- (1) Supercritical  $\text{CO}_2$  can liberate diesel-range *n*-aliphatic hydrocarbons from high-maturity shale at estimated *in situ* reservoir pressure and temperature conditions. Extraction yields range between 0.3 and 12 mg HC/g TOC.
- (2) No strong correlation is found between sieve size and extracted hydrocarbon yield. However, hydrocarbon yield is highest from the 250–125  $\mu\text{m}$  sieve size fraction in all sample extracts. The significance of the effect of sieve size on yield may have been limited given the low sieve size ranges of the extracted shale particles.
- (3) Mineralogy appears to have no effect on the observed differences in extraction yield (abundance or distribution of hydrocarbons) among cores.
- (4) Extraction yield increases with increasing surface area, regardless of sieve size range. However, given  $\text{N}_2$ 's inability to access micropores (<2 nm) within shale matrices, use of  $\text{N}_2$  as opposed to  $\text{CO}_2$  to measure surface area may be obscuring a stronger correlation between extraction yield and exposed surface area.
- (5) Surface area and extraction yield both increase with an increase in TOC content, reflecting the contribution of organic matter to pores and exposed internal surface areas within the shale matrix that are accessible to the extraction solvent, supercritical  $\text{CO}_2$ .

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## Notes

**Disclosure.** Any use of trade, product, or firm names is for descriptive purposes only and does not imply endorsement by the U.S. Government or the University of Maryland. The authors declare no competing financial interest.

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